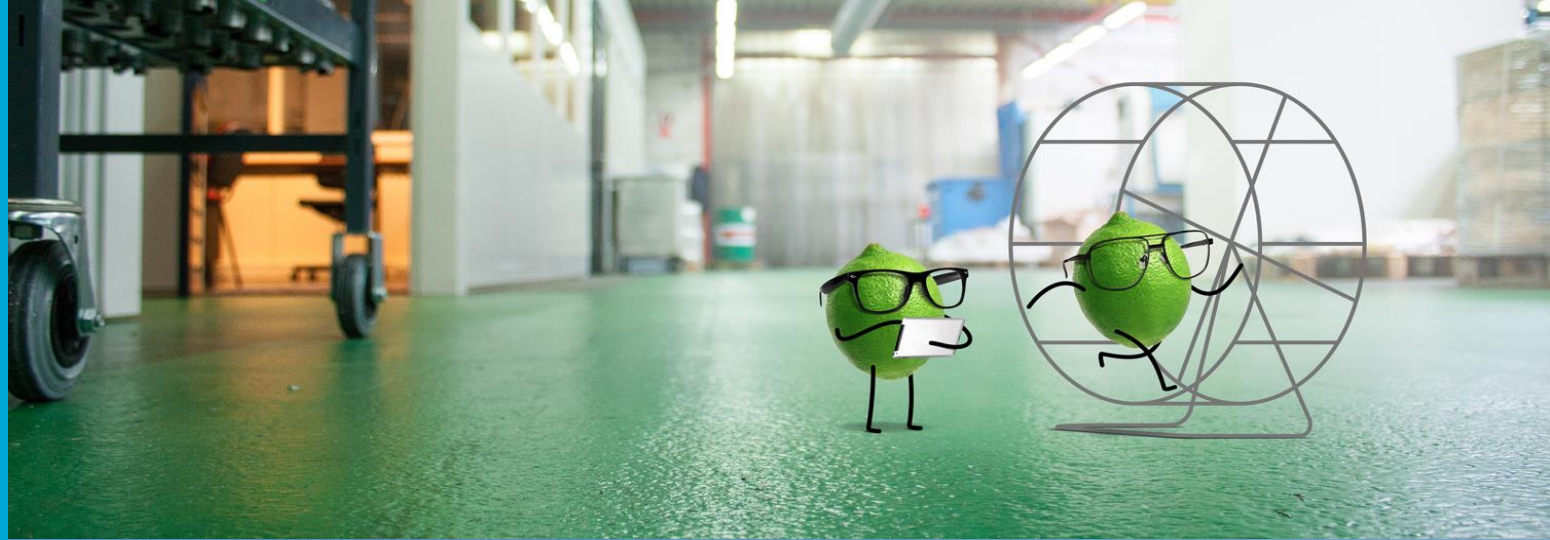


# Data Driven Turbulence Modeling

Midterm Presentation:  
Elske van Leeuwen

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# Turbulence and its Modeling

# Turbulence

- Chaotic behavior of fluid flow
- Modeling improves the design of technological applications

- Navier-Stokes equations describe the motion of a flow

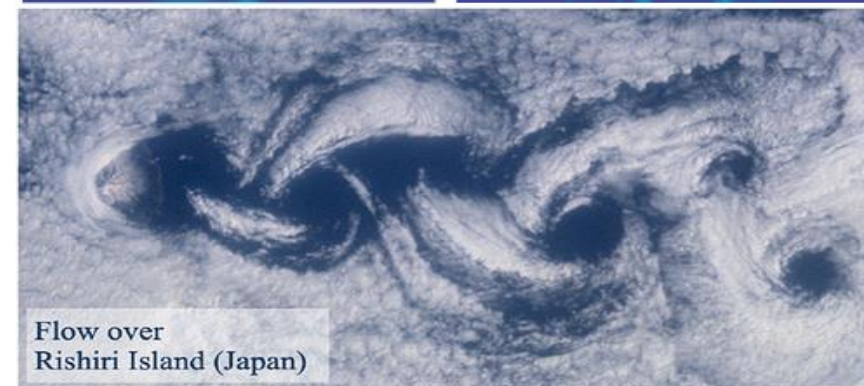
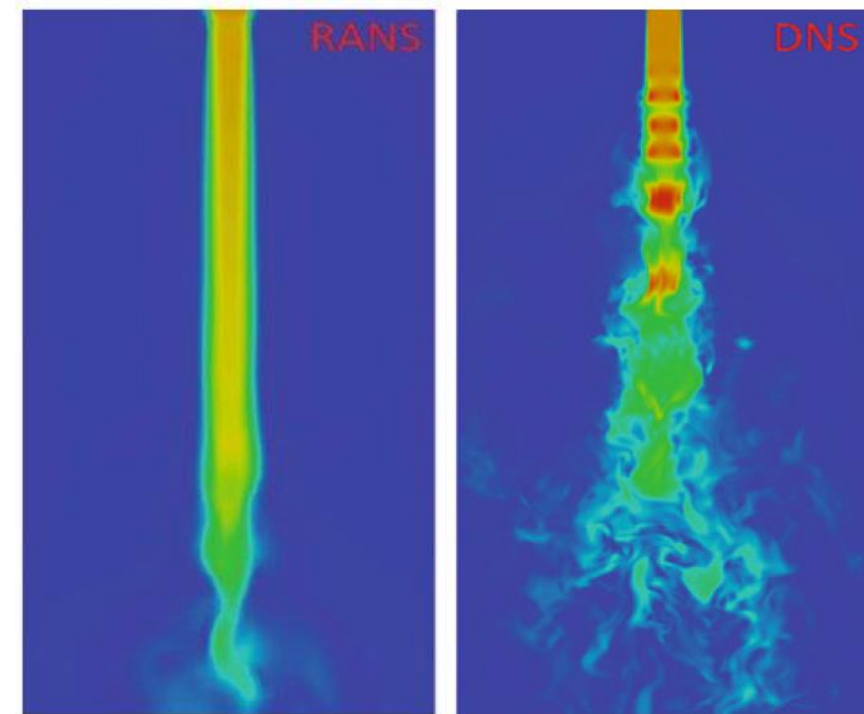
- $$\rho \left( \frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = \frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2}$$





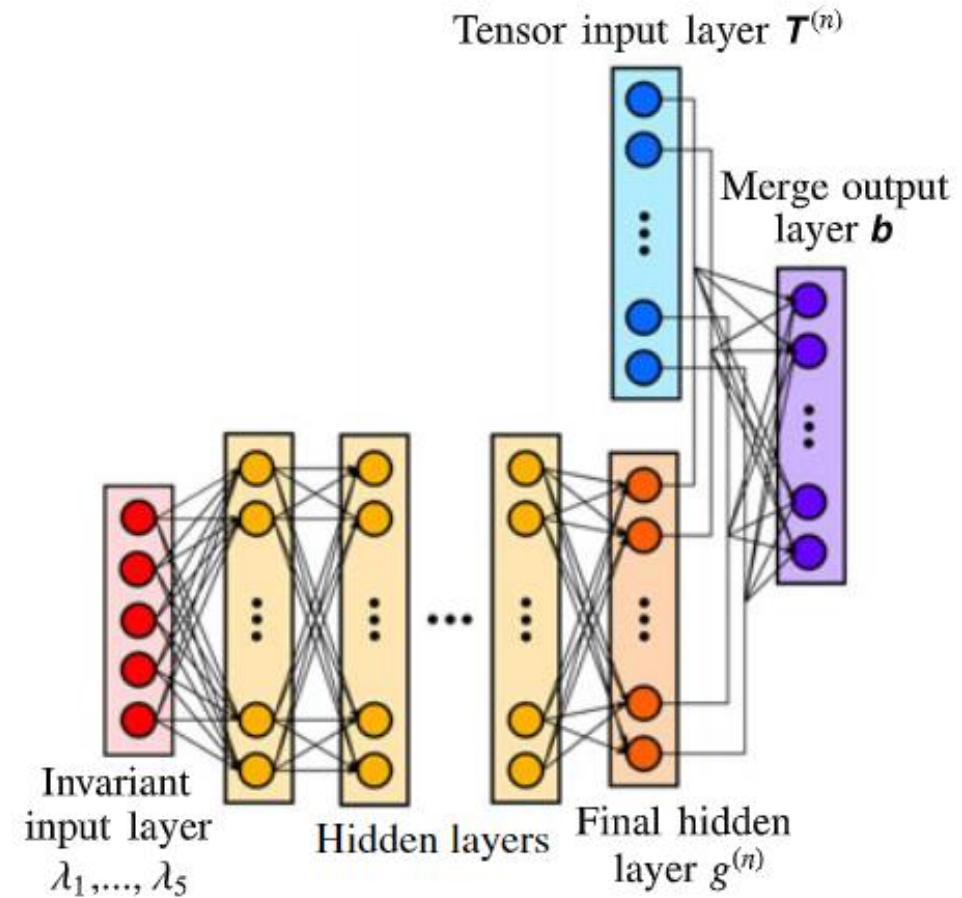
# Turbulence Modeling

- Direct Numerical Simulations (DNS)
  - High accuracy
  - High computational complexity
- Reynolds Average Navier Stokes (RANS) models
  - Low accuracy
  - Low computation
  
- Interest in Machine Learning increased:
  - ML is able to find patterns
  - More data available since the of computational power has increased



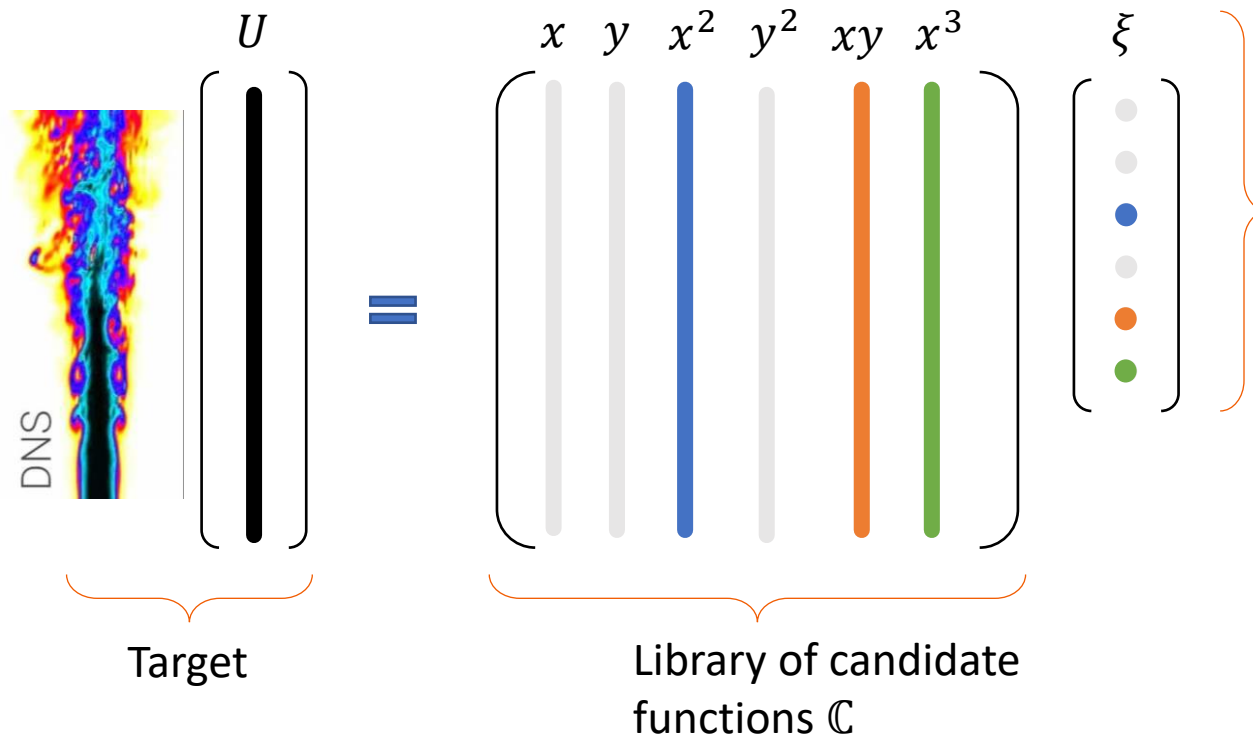
# Challenges ML in Turbulence Modeling

- Interpretability
- Generalizability
- Simplicity
- Physically Informed
- Integration with CFD Solvers



# Sparse Symbolic Regression

- Finds a mathematical expression for a quantity of interest
- Requires a library of candidate functions
- Selects function with sparse regression techniques



# Sparse Symbolic Regression

- Interpretable
- Physics informed
- Efficient
- Simple
- Integration with CFD solvers (OpenFoam) possible and “easy”

# Objectives and Questions



# Objective

- Develop a data-driven turbulence model using sparse symbolic regression to improve a RANS turbulence model, which contains physical knowledge and should be interpretable, generalizable and robust

# Questions

- Which features are the most relevant?
- How can physical knowledge be included?
- Which sparse symbolic regression technique finds the best performing algebraic model?
- How does the obtained turbulence model perform in terms of robustness, generalizability and interpretability?

# Methodology

# RANS Turbulence Modeling

- Filling in  $U = \bar{U} + U'$  in the NS equation (Reynolds' decomposition):

- NS: 
$$\frac{DU_i}{Dt} = -\frac{1}{\rho} \frac{\partial P}{\partial x_i} + \nu \frac{\partial^2 U_i}{\partial x_j^2}$$

- RANS: 
$$\frac{D\bar{U}_i}{Dt} = -\frac{1}{\rho} \frac{\partial P}{\partial x_i} + \nu \frac{\partial^2 \bar{U}_i}{\partial x_j^2} - \frac{\partial}{\partial x_j} (\overline{U'_i U'_j})$$

- Reynolds stress =  $\overline{U'_i U'_j}$

- Requires modeling

- Boussinesq:  $\overline{U'_i U'_j} = -2\nu_t S_{ij} + \frac{2}{3} k \delta_{ij}$

$$S_{ij} = \frac{1}{2} \left( \frac{\partial \bar{U}_i}{\partial x_j} + \frac{\partial \bar{U}_j}{\partial x_i} \right)$$

# Subject of Modeling

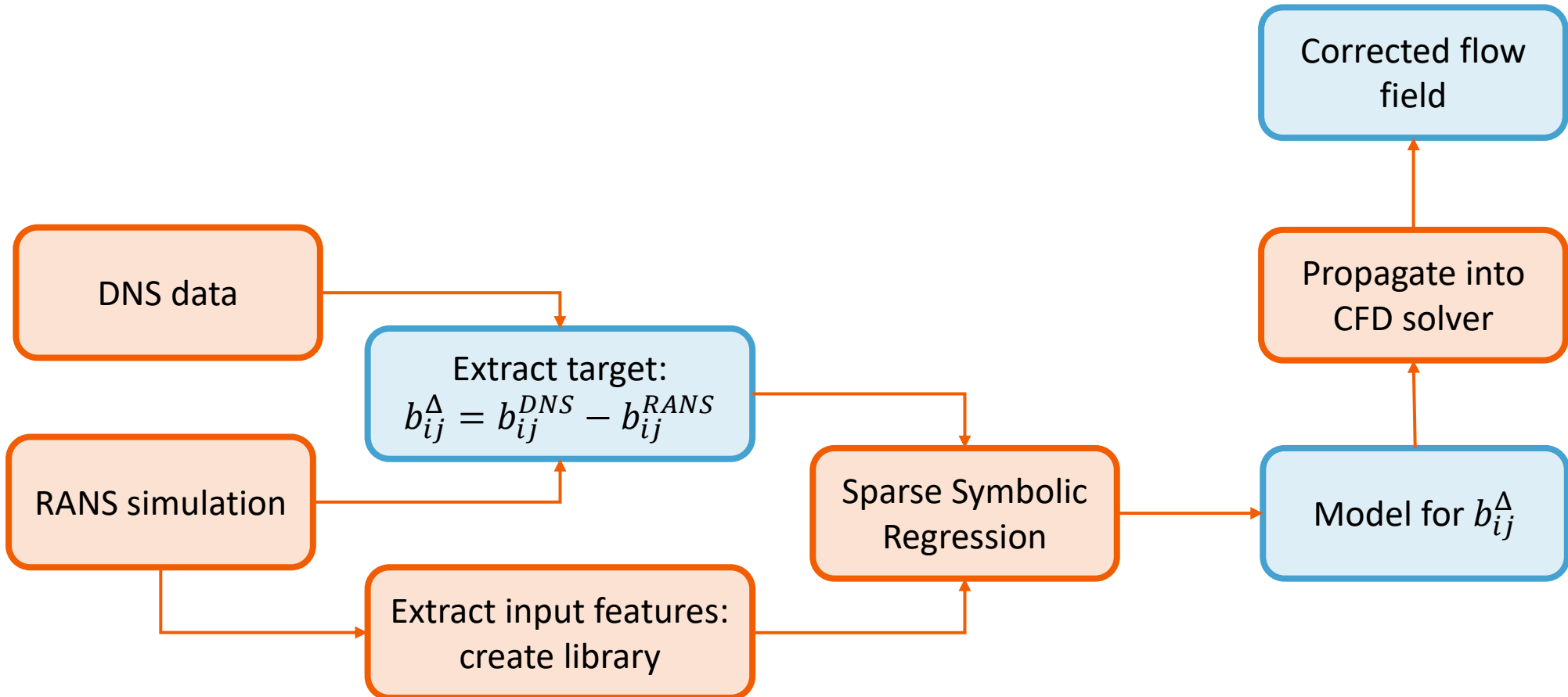
- $-\overline{U'_i U'_j} = 2k \left( b_{ij} + \frac{1}{3} \delta_{ij} \right)$
- Here,  $b_{ij}$  is the anisotropic stress tensor:
  - Boussinesq:  $b_{ij} = -\frac{\nu_t}{k} S_{ij}$
  - Pope:  $b_{ij}(\hat{S}_{ij}, \hat{R}_{ij}) = \sum_{n=1}^{10} G^{(n)}(\lambda_1, \dots, \lambda_2) T_{ij}^{(n)}$ 
    - $S_{ij} = \frac{1}{2} \left( \frac{\partial \bar{U}_i}{\partial x_j} + \frac{\partial \bar{U}_j}{\partial x_i} \right)$
    - $R_{ij} = \frac{1}{2} \left( \frac{\partial \bar{U}_i}{\partial x_j} - \frac{\partial \bar{U}_j}{\partial x_i} \right)$
- Split into linear and nonlinear portions:

$T_{ij}^{(1)} = S_{ij}$	$T_{ij}^{(6)} = R_{ik} R_{kl} S_{lj} + S_{ik} R_{kl} R_{lj} - \frac{2}{3} S_{pk} R_{kl} R_{lp} \delta_{ij}$
$T_{ij}^{(2)} = S_{ik} R_{kj} - R_{ik} S_{kj}$	$T_{ij}^{(7)} = R_{ik} S_{kl} R_{lp} R_{pj} - R_{ik} R_{kl} S_{lp} R_{pj}$
$T_{ij}^{(3)} = S_{ik} S_{kj} - \frac{1}{3} S_{lk} S_{kl} \delta_{ij}$	$T_{ij}^{(8)} = S_{ik} R_{kl} S_{lp} S_{pj} - S_{ik} S_{kl} R_{lp} S_{pj}$
$T_{ij}^{(4)} = R_{ik} R_{kj} - \frac{1}{3} R_{lk} R_{kl} \delta_{ij}$	$T_{ij}^{(9)} = R_{ik} R_{kl} S_{lp} S_{pj} + S_{ik} S_{kl} R_{lp} R_{pj} - \frac{2}{3} S_{qk} S_{kl} R_{lp} R_{pq}$
$T_{ij}^{(5)} = R_{ik} S_{kl} S_{lj} - S_{ik} S_{kl} R_{lj}$	$T_{ij}^{(10)} = R_{ik} S_{kl} S_{lp} R_{pq} R_{qj} - R_{ik} R_{kl} S_{lp} S_{pq} R_{qj}$

$$b_{ij} = \underbrace{-\frac{\nu_t}{k} \hat{S}_{ij}}_{\text{linear}} + \underbrace{b_{ij}^\Delta}_{\text{non-linear}}$$

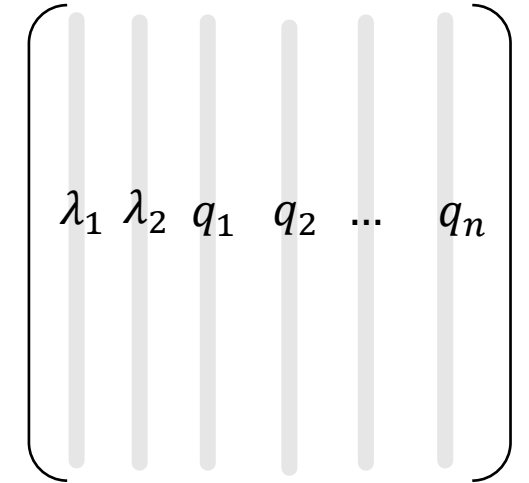


# Modeling Overview



# Library of Candidate Functions

- Select appropriate features
- Create more complex functions by multiplying the features with each other
- Multiply each function with the tensor bases  $T_{ij}^{(n)}$



$T_{ij}^{(1)} = S_{ij}$	$T_{ij}^{(6)} = R_{ik}R_{kl}S_{lj} + S_{ik}R_{kl}R_{lj} - \frac{2}{3}S_{pk}R_{kl}R_{lp}\delta_{ij}$
$T_{ij}^{(2)} = S_{ik}R_{kj} - R_{ik}S_{kj}$	$T_{ij}^{(7)} = R_{ik}S_{kl}R_{lp}R_{pj} - R_{ik}R_{kl}S_{lp}R_{pj}$
$T_{ij}^{(3)} = S_{ik}S_{kj} - \frac{1}{3}S_{lk}S_{kl}\delta_{ij}$	$T_{ij}^{(8)} = S_{ik}R_{kl}S_{lp}S_{pj} - S_{ik}S_{kl}R_{lp}S_{pj}$
$T_{ij}^{(4)} = R_{ik}R_{kj} - \frac{1}{3}R_{lk}R_{kl}\delta_{ij}$	$T_{ij}^{(9)} = R_{ik}R_{kl}S_{lp}S_{pj} + S_{ik}S_{kl}R_{lp}R_{pj} - \frac{2}{3}S_{qk}S_{kl}R_{lp}R_{pq}$
$T_{ij}^{(5)} = R_{ik}S_{kl}S_{lj} - S_{ik}S_{kl}R_{lj}$	$T_{ij}^{(10)} = R_{ik}S_{kl}S_{lp}R_{pq}R_{qj} - R_{ik}R_{kl}S_{lp}S_{pq}R_{qj}$

# Sparse Symbolic Regression

## Two step modeling

### 1. Model Discovery

- Standardization of the features
- Lasso Regression:  $\xi = \operatorname{argmin}_{\xi} \|U - C\xi\|_2^2 + \lambda \|\xi\|_1$
- Selecting the 'active' features

### 2. Model Inference

- No standardization of the features
- Only using the selected features
- Ridge Regression:  $\xi = \operatorname{argmin}_{\xi} \|U - C\xi\|_2^2 + \lambda \|\xi\|_2^2$
- Calibration of the coefficient

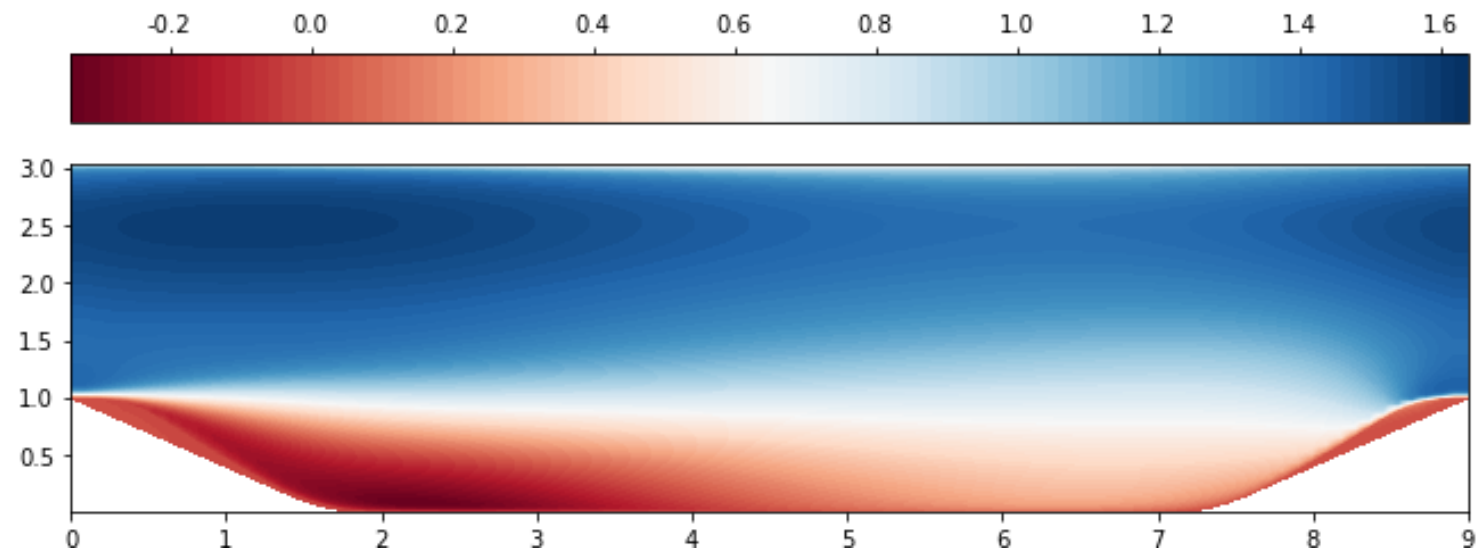
# Case Studies

- Channel Flow
- Periodic Hill
- Square Duct
- Taylor Couette flow
- Industrial Problem: Vortex Gripper

# Some first results



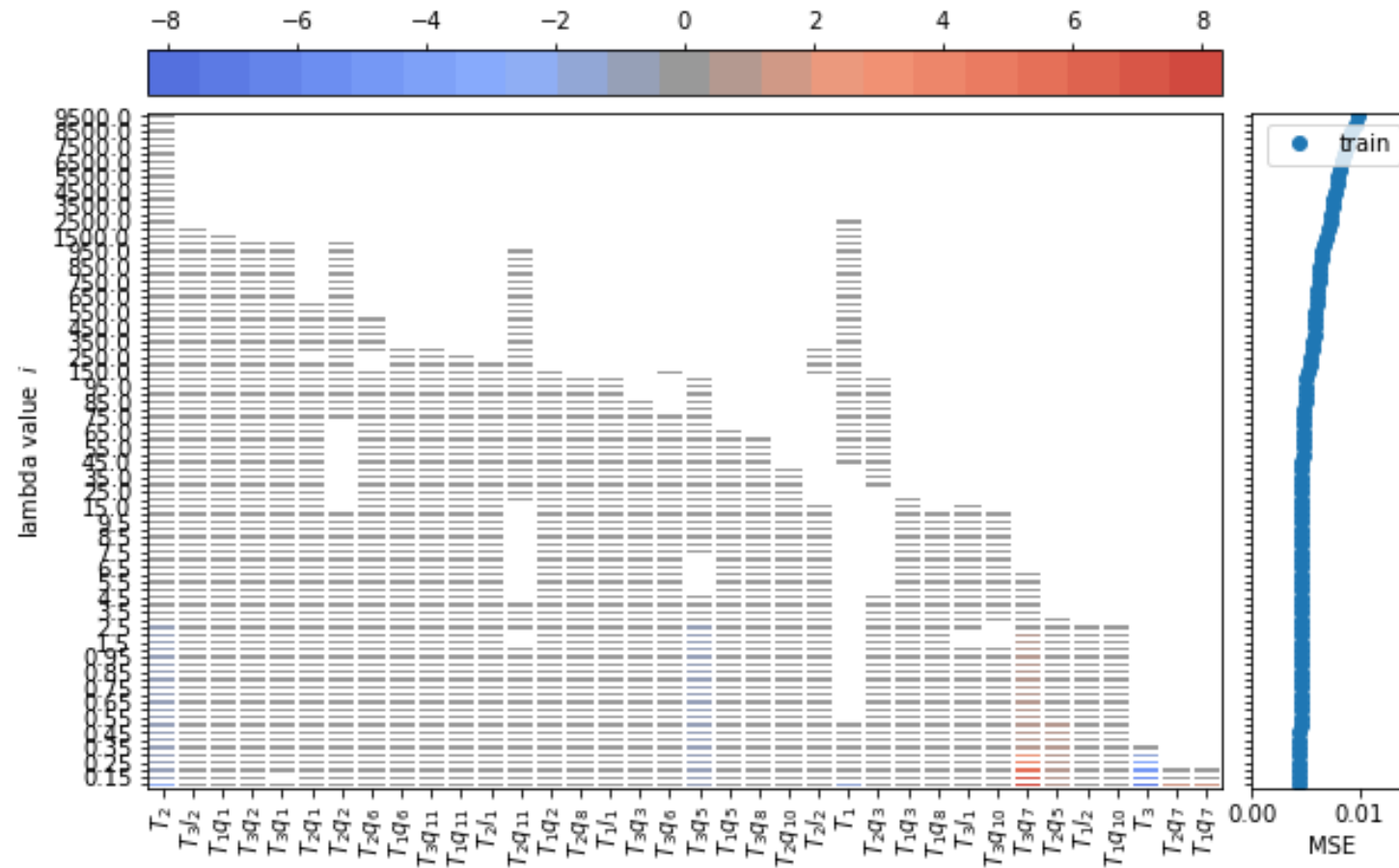
# Periodic Hill



# Model Discovery

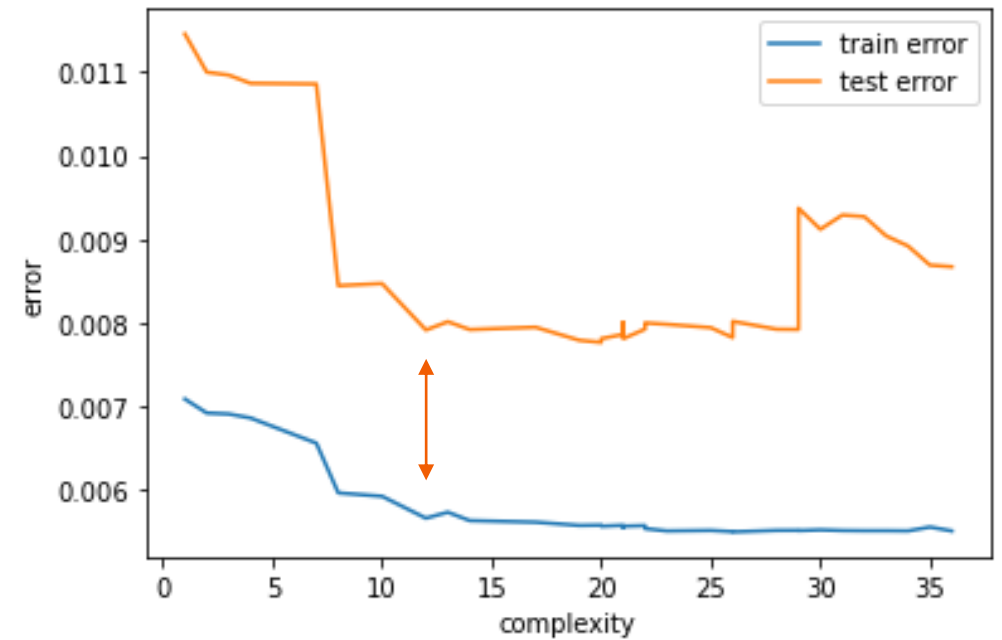
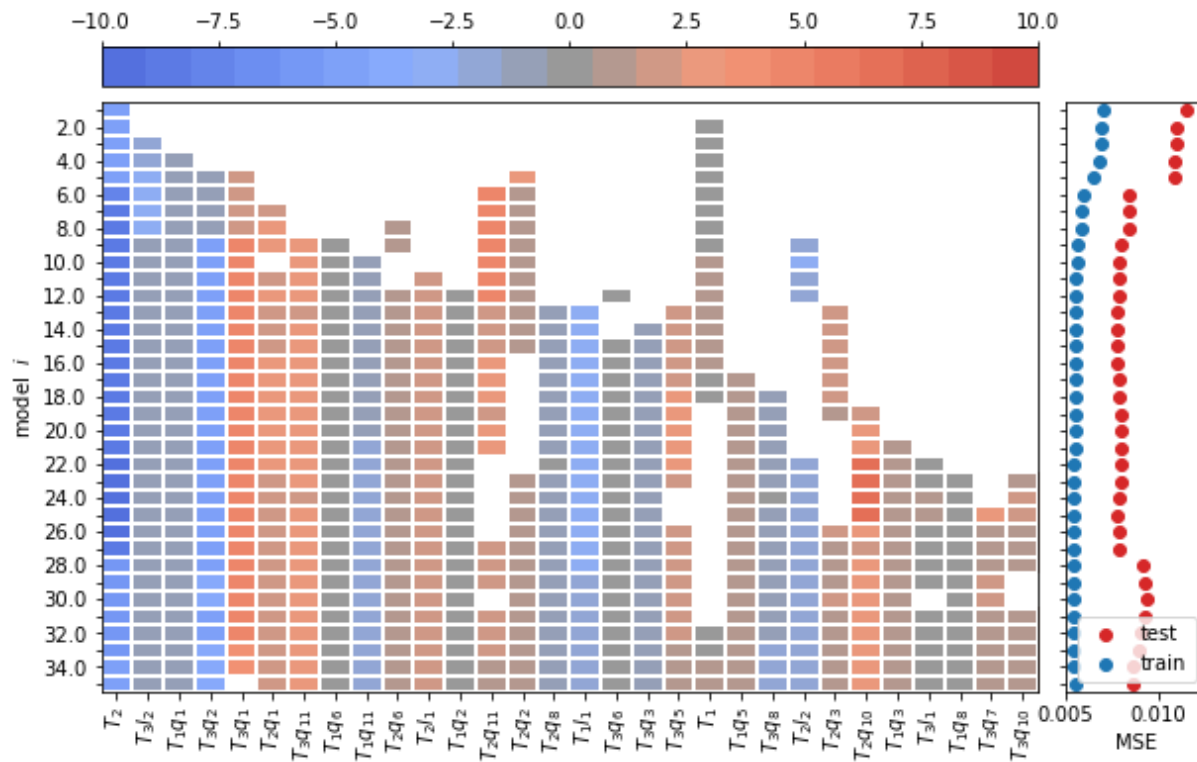
- Lasso Regression:  $\xi = \min \|b^* - C\xi\|_2^2 + \lambda \|\xi\|_1$

index	Features
$q_1$	$\frac{1}{2}(\ R\ ^2 - \ S\ ^2)$
$q_2$	$k$
$q_3$	$\min(\frac{\sqrt{kd}}{50\nu}, 2)$
$q_4$	$\bar{u}_i \frac{\partial p}{\partial x_k}$
$q_5$	$k/\epsilon$
$q_6$	$\bar{u}_i \frac{\partial k}{\partial x_i}$
$q_7$	$\ \bar{u}_i' \bar{u}_j'\ $
$q_8$	$\sqrt{\frac{\partial p}{\partial x_i} \frac{\partial p}{\partial x_i}}$
$q_9$	$ \bar{u}_i \bar{u}_j \frac{\partial \bar{u}_i}{\partial x_j} $
$q_{10}$	$f_1$
$q_{11}$	$f_1^2$
$l_1$	$\text{trace}(S^2)$
$l_2$	$\text{trace}(\Omega^2)$



# Model Inference

- Ridge regression:  $\xi = \min \|b^* - \mathbb{C}\xi\|_2^2 + \lambda \|\xi\|_2^2$ ,
  - $\lambda = 0.1$
- Selecting models:
  - Trade-off between complexity and accuracy

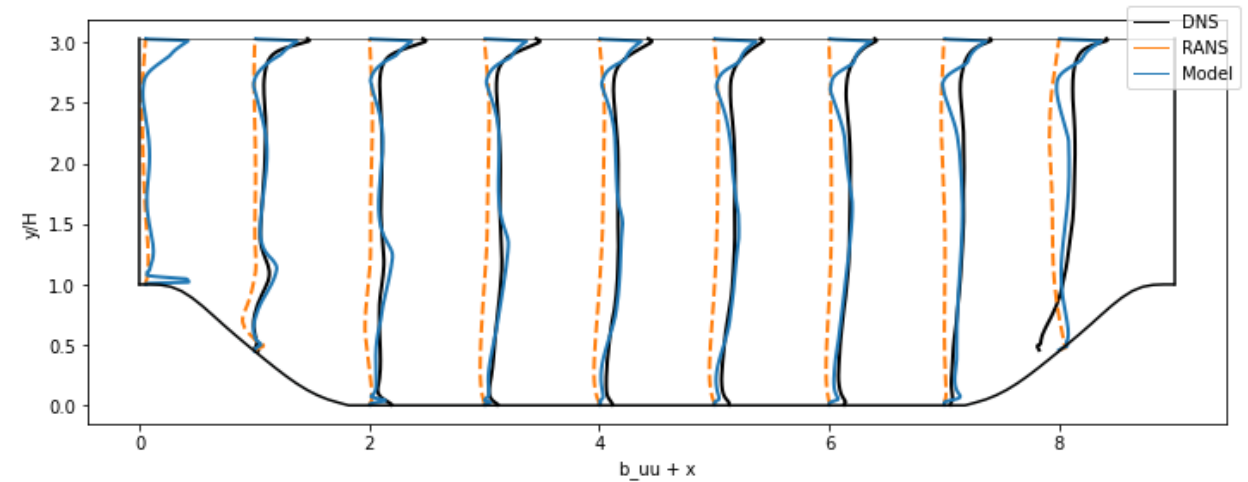
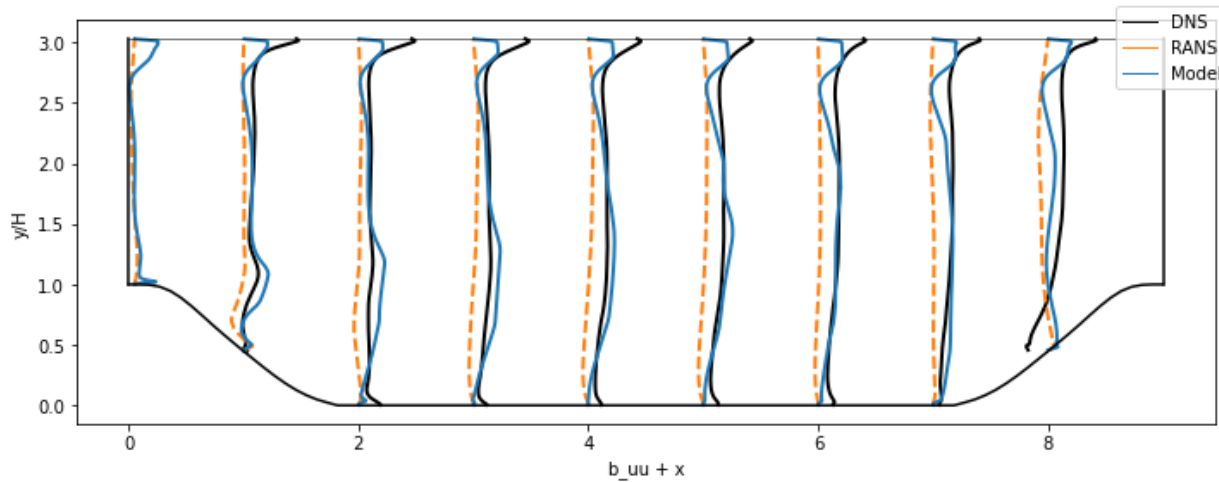


# Result of selected models

Anisotropic stress:  $b_{ij} = \frac{v_t}{k} S_{ij} + b_{ij}^*$

- Simple:  $b_{ij}^* = -4.3 * T_2$

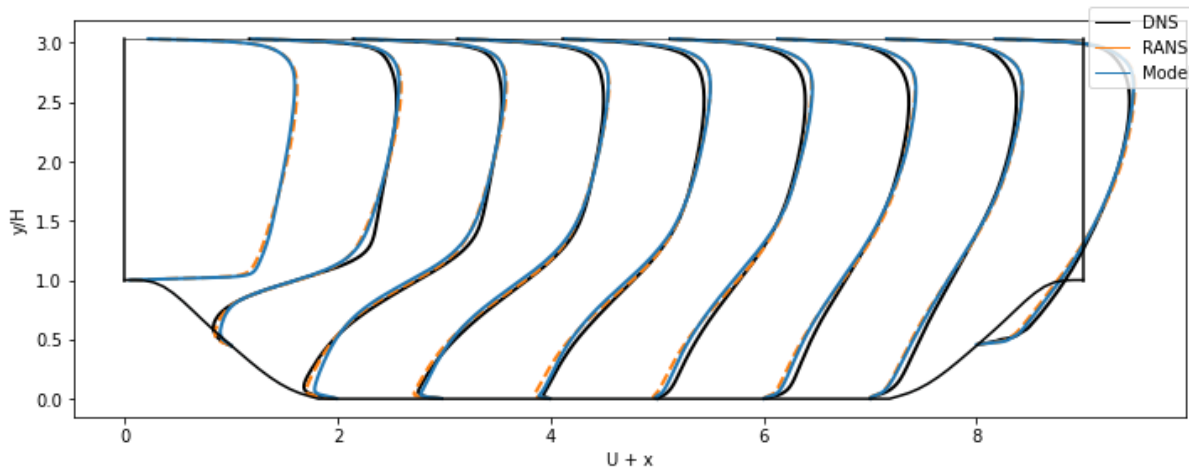
More complex:  $b_{ij}^* = (1.72q_1 - 0.71q_{11} + 0.08q_6 + 0.80)T_1$   
 $+ (-2.55l_2 + 4.71q_{11} + 0.72q_2 - 8.20)T_2$   
 $+ (-1.24l_2 + 4.51q_1 + 3.23q_{11} - 4.56q_2)T_3$



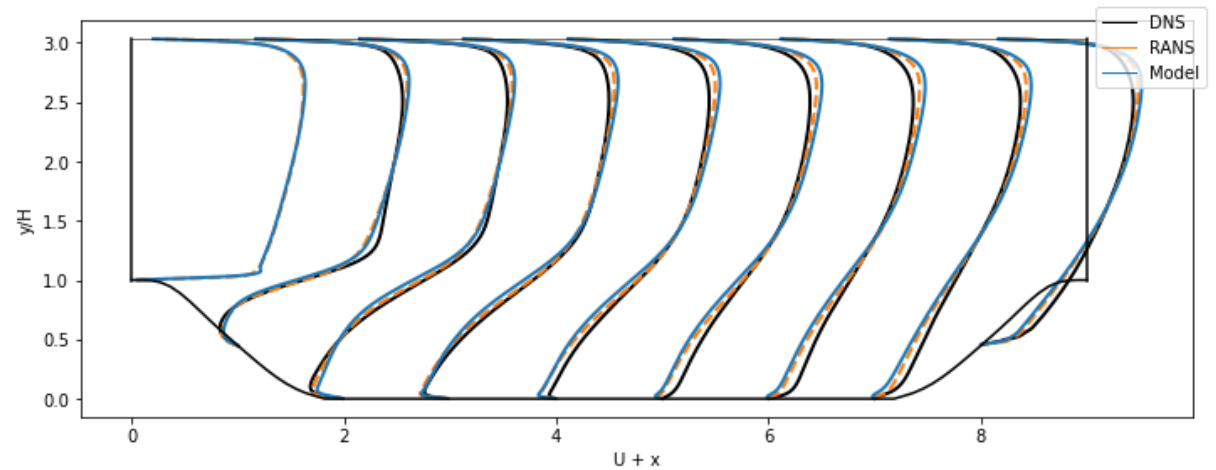
# Model Propagation

## Streamwise velocity profiles

- Simple:  $b_{ij}^* = -4.3 * T_2$



- More complex:  $b_{ij}^* = (1.72q_1 - 0.71q_{11} + 0.08q_6 + 0.80)T_1$   
 $+ (-2.55l_2 + 4.71q_{11} + 0.72q_2 - 8.20)T_2$   
 $+ (-1.24l_2 + 4.51q_1 + 3.23q_{11} - 4.56q_2)T_3$





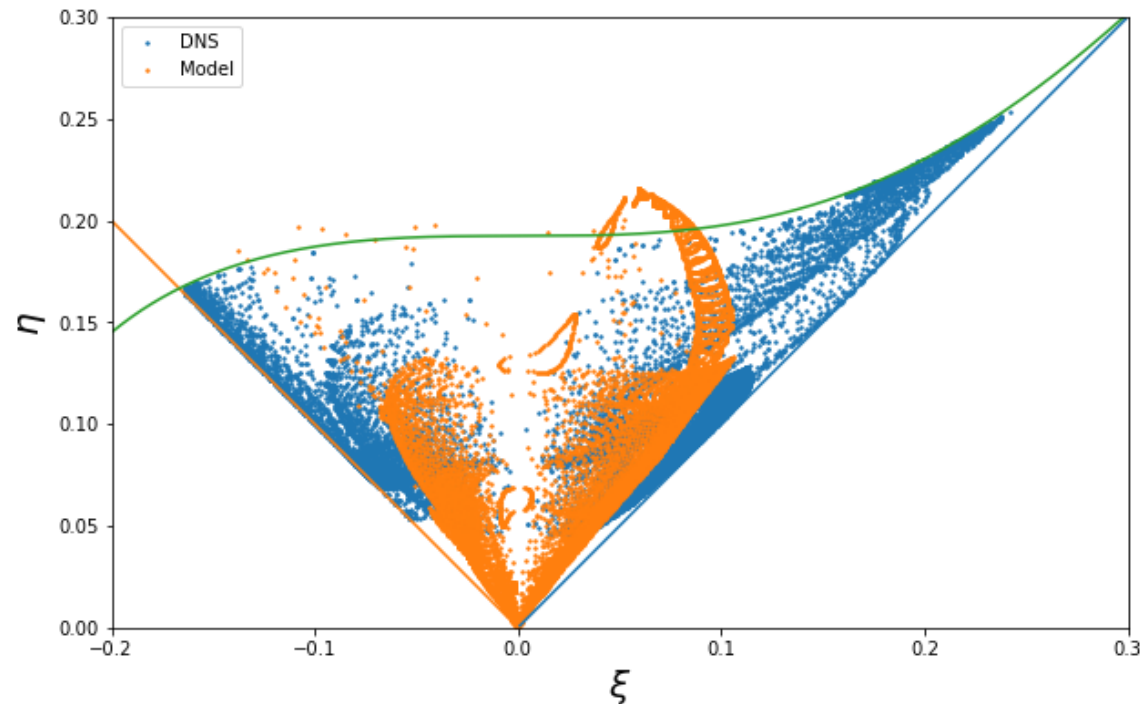
# Constraints

For realizable flows:  $b_{ii} \in \left[-\frac{1}{3}, \frac{2}{3}\right]$  and  $b_{ij} \in \left[-\frac{1}{2}, \frac{1}{2}\right]$

Creating a Lumley triangle using:  $\zeta^3 = b_{ij}b_{in}b_{jn}/2$  and  $\eta^2 = -\frac{b_{ij}b_{ji}}{2}$

Values of  $\zeta$  and  $\eta$  should be inside the triangle

Adding constraints in regression function could enforce the realizability



# Intermediate Conclusions

# Intermediate conclusions

- Frame-work to discover models with sparse symbolic regression
- Possible to add constraints
- No improvement of the velocity profiles yet

What's left?

## To do:

- Finding a good model that improves the velocity
- Research different regression functions
- Research the effect of adding constraints to the regression functions
- Perform the other test cases



To be continued...  
Questions?